



Institute of Aeronautics and Applied Mechanics

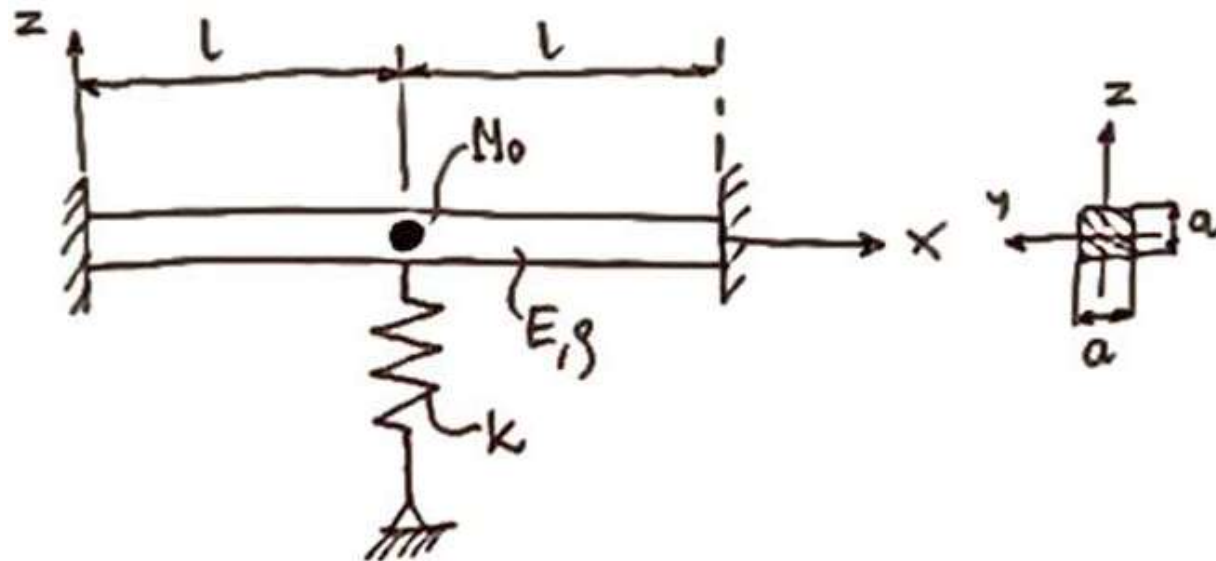
# Finite element method 2 (FEM 2)

Example of modal analysis

11.2021

**Example.** Build a finite element model and write the set of equations for modal analysis of a 2D structure consisting of a beam, spring and mass  $M_0$ . The beam is represented by 2 finite elements.

- Find natural frequencies ( $f_1, f_2$ ) and corresponding eigenvectors. Draw the mode shapes.
- Calculate the minimum value of spring stiffness, so that the mode shape without the translation of mass  $M_0$  becomes the first vibration mode.



$$E = 2 \cdot 10^5 \text{ MPa}$$

$$L = 1000 \text{ mm}$$

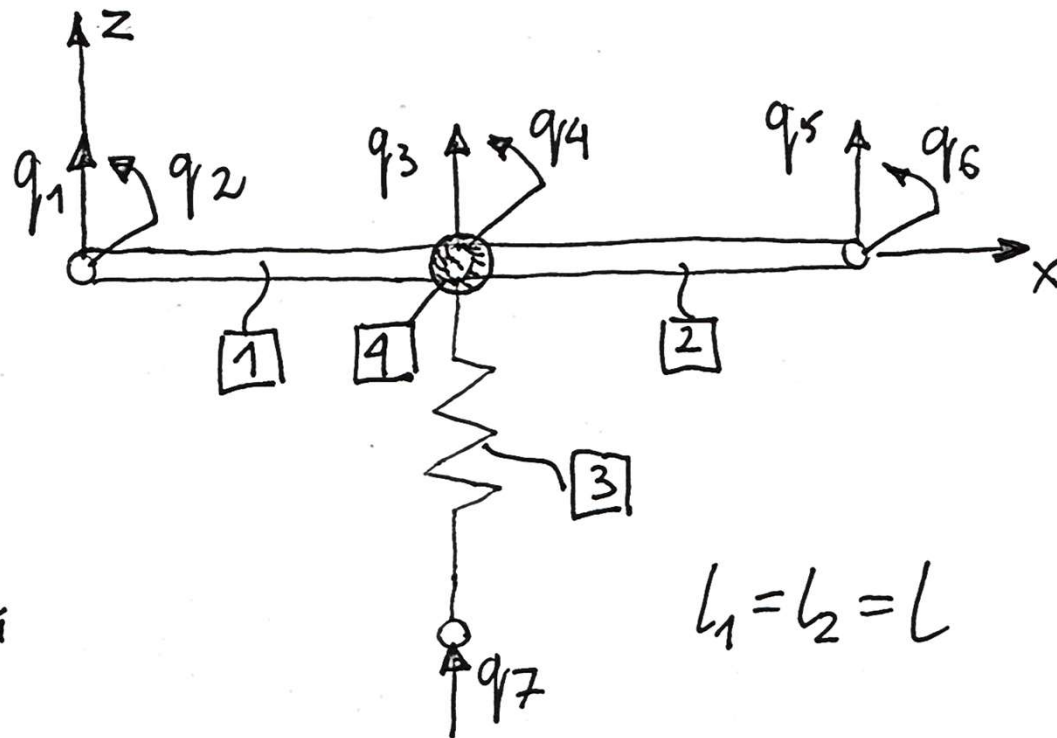
$$a = 40 \text{ mm}$$

$$\rho = 7800 \frac{\text{kg}}{\text{m}^3}$$

$$M_0 = 20 \text{ kg}$$

$$k = 5000 \frac{\text{N}}{\text{mm}}$$

$$A = a^2, \quad J_y = \frac{a^4}{12}$$



$$L_1 = L_2 = L$$

GLOBAL VECTOR OF NODAL PARAMETERS :

$$\underset{1 \times 7}{[q]} = [q_1, q_2, q_3, q_4, q_5, q_6, q_7]$$

LOCAL STIFFNESS MATRICES :

$$[k]_1 = [k]_2 = \frac{2EJ_y}{l^3} \cdot \begin{bmatrix} 6 & 3l & -6 & 3l \\ 3l & 2l^2 & -3l & l^2 \\ -6 & -3l & 6 & -3l \\ 3l & l^2 & -3l & 2l^2 \end{bmatrix} = \frac{Ea^4}{6l^3} \cdot \begin{bmatrix} 6 & 3l & -6 & 3l \\ 3l & 2l^2 & -3l & l^2 \\ -6 & -3l & 6 & -3l \\ 3l & l^2 & -3l & 2l^2 \end{bmatrix}$$

$$[k]_3 = \begin{bmatrix} k & -k \\ -k & k \end{bmatrix}, \quad [k]_4 = \begin{bmatrix} 0 \end{bmatrix}$$

$2 \times 2$                        $(1 \times 1)$                        $(1 \times 1)$

LOCAL MASS MATRICES :

$$[m]_1 = [m]_2 = \frac{\rho a^2 l}{420} \cdot \begin{bmatrix} 156 & 22l & 54 & -13l \\ 22l & 4l^2 & 13l & -3l \\ 54 & 13l & 156 & -22l \\ -13l & -3l & -22l & 4l^2 \end{bmatrix}$$

$$[m]_3 = \begin{bmatrix} 0 & 0 \\ 0 & 0 \end{bmatrix}, \quad [m]_4 = \begin{bmatrix} M_0 \end{bmatrix}$$

$2 \times 2$                        $(1 \times 1)$                        $(1 \times 1)$

EXTENDED STIFFNESS MATRICES.

$$[k]_1^* = \begin{bmatrix} \text{shaded } [k]_1 & 0 & 0 & 0 \\ \text{shaded } [k]_1 & 0 & 0 & 0 \\ \text{shaded } [k]_1 & 0 & 0 & 0 \\ \text{shaded } [k]_1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix}$$

4x4

$$; [k]_2^* = \begin{bmatrix} 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & \text{shaded } [k]_2 & 0 & 0 & 0 & 0 \\ 0 & 0 & \text{shaded } [k]_2 & 0 & 0 & 0 & 0 \\ 0 & 0 & \text{shaded } [k]_2 & 0 & 0 & 0 & 0 \\ 0 & 0 & \text{shaded } [k]_2 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 \end{bmatrix}$$

1x4

$$[k]_3^* = \begin{bmatrix} 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & k & 0 & 0 & 0 & -k \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & -k & 0 & 0 & 0 & k \end{bmatrix}$$

$$; [k]_4^* = [0]$$

7x7

# EXTENDED MASS MATRICES

$$[m]_{7 \times 7}^* = \begin{bmatrix} \boxed{[m]_{4 \times 4}^*} & \begin{matrix} 0 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{matrix} \\ \begin{matrix} 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 \end{matrix} & \end{bmatrix}$$

;

$$[m]_{7 \times 7}^* = \begin{bmatrix} \begin{matrix} 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & \boxed{[m]_{4 \times 4}^*} & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 \end{matrix} & \end{bmatrix}$$

$$[m]_{7 \times 7}^* = [0]_{7 \times 7}$$

,

$$[m]_{7 \times 7}^* = \begin{bmatrix} 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & M_0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 \end{bmatrix}$$



BOUNDARY CONDITIONS

$$q_1 = 0, q_2 = 0, q_5 = 0, q_6 = 0, q_7 = 0$$

SET OF EQUATIONS :

$$\left( \begin{array}{c|c} K_{33-1} + K_{11-2} + k & K_{34-1} + K_{12-2} \\ \hline K_{43-1} + K_{21-2} & K_{44-1} + K_{22-2} \end{array} \right)$$

$$- \omega^2 \left( \begin{array}{c|c} m_{33-1} + m_{11-2} + M_0 & m_{34-1} + m_{12-2} \\ \hline m_{43-1} + m_{21-2} & m_{44-1} + m_{22-2} \end{array} \right) \cdot \begin{Bmatrix} q_3 \\ q_4 \end{Bmatrix} = \begin{Bmatrix} 0 \\ 0 \end{Bmatrix}$$



$$k_{33-1} + k_{11-2} + k = \frac{6Ea^4}{6l^3} + \frac{6Ea^4}{6l^3} + k = \frac{2Ea^4}{l^3} + k$$

$$k_{34-1} + k_{12-2} = -\frac{3l \cdot Ea^4}{6l^3} + \frac{3l Ea^4}{6l^3} = 0 = k_{43-1} + k_{21-2}$$

$$k_{44-1} + k_{22-2} = \frac{2l^2 \cdot Ea^4}{6l^3} + \frac{2l^2 Ea^4}{6l^3} = \frac{2Ea^4}{3l}$$

$$m_{33-1} + m_{11-2} + M_0 = \frac{156 \cdot \rho a^2 l}{420} + \frac{156 \rho a^2 l}{420} + M_0 = \frac{26 \rho a^2 l}{35} + M_0$$

$$m_{34-1} + m_{12-2} = \frac{-22l \cdot \rho a^2 l}{420} + \frac{22l \cdot \rho a^2 l}{420} = 0 = m_{43-1} + m_{21-2}$$

$$m_{44-1} + m_{22-2} = \frac{4l^2 \rho a^2 l}{420} + \frac{4l^2 \rho a^2 l}{420} = \frac{2 \rho a^2 l^3}{105}$$

$$\begin{pmatrix} \frac{2Ea^4}{l^3} + k & 0 \\ 0 & \frac{2Ea^4}{3l} \end{pmatrix} - \omega^2 \begin{pmatrix} \frac{26 \rho a^2 l}{35} + M_0 & 0 \\ 0 & \frac{2 \rho a^2 l^3}{105} \end{pmatrix} \cdot \begin{Bmatrix} q_3 \\ q_4 \end{Bmatrix} = \begin{Bmatrix} 0 \\ 0 \end{Bmatrix}$$

$$\det \left( \begin{matrix} [K] & \\ & -\omega^2 [M] \end{matrix} \right) = 0$$

$$M_0 = 20 \text{ kg} = 20 \frac{\text{kg} \cdot \text{m}}{\text{s}^2} \cdot \frac{\text{s}^2}{\text{m}} = 20 \frac{\text{Ns}^2}{1000 \text{ mm}} = 0.02 \frac{\text{Ns}^2}{\text{mm}} \quad f_1 = 72.2 \text{ Hz}$$

$$\rho = 7800 \frac{\text{kg}}{\text{m}^3} = 7800 \frac{\text{kg} \cdot \text{m}}{\text{s}^2} \cdot \frac{\text{s}^2}{\text{m} \cdot \text{m}^3} = 7.8 \cdot 10^{-9} \frac{\text{Ns}^2}{\text{mm}^4}$$

$$\left\{ \left( \frac{2Ea^4}{l^3} + k \right) - \omega^2 \left( \frac{269a^2l}{35} + M_0 \right) \right\} \cdot \left( \frac{2Ea^4}{3l} - \omega^2 \cdot \frac{29a^2l^3}{105} \right) = 0.$$

$$\begin{aligned} \hookrightarrow \omega_1 &= \sqrt{\frac{\frac{2Ea^4}{l^3} + k}{\frac{269a^2l}{35} + M_0}} = \\ &= 453.7 \text{ 1/s} \end{aligned}$$

$$f_1 = 72.2 \text{ Hz}$$

$$\begin{aligned} \hookrightarrow \omega_2 &= \sqrt{\frac{\frac{2Ea^4}{3l}}{\frac{29a^2l^3}{105}}} = \\ &= \frac{a}{l^2} \cdot \sqrt{\frac{35E}{9}} = 1198.3 \text{ 1/s} \end{aligned}$$

$$f_2 = 190.71 \text{ Hz}$$

## EIGEN VECTORS

NEW CONSTANTS :

$$\Phi(\omega_i) = \frac{2Ea^4}{l^3} + k - \omega_i^2 \left( \frac{26\varrho a^2 l}{35} + M_0 \right)$$

$$\Psi(\omega_i) = \frac{2Ea^4}{3l} - \omega_i^2 \cdot \frac{2\varrho a^2 l^3}{105}$$

$$\begin{cases} \Phi(\omega_i) \cdot q_3(\omega_i) + 0 \cdot q_4(\omega_i) = 0 \\ 0 \cdot q_3(\omega_i) + \Psi(\omega_i) \cdot q_4(\omega_i) = 0 \end{cases}$$

$\underline{I} + \underline{II} :$

$$\Phi(\omega_i) \cdot q_3(\omega_i) + \Psi(\omega_i) \cdot q_4(\omega_i) = 0$$

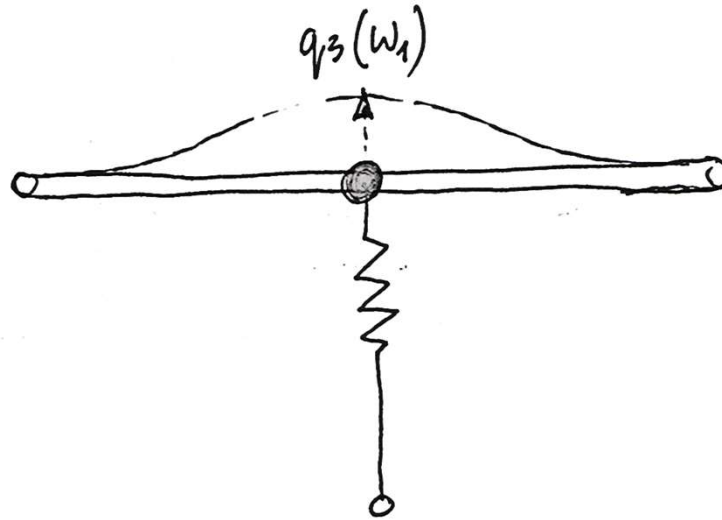
for  $\omega_1$  :  $\Phi(\omega_1) = 0$  ,  $\Psi(\omega_1) \neq 0$

$$0 \cdot q_3(\omega_1) + \Psi(\omega_1) \cdot q_4(\omega_1) = 0$$

$\hookrightarrow$  any real value       $\hookrightarrow = 0$

1st vibration  
mode

$$f_1 = 72.2 \text{ Hz}$$

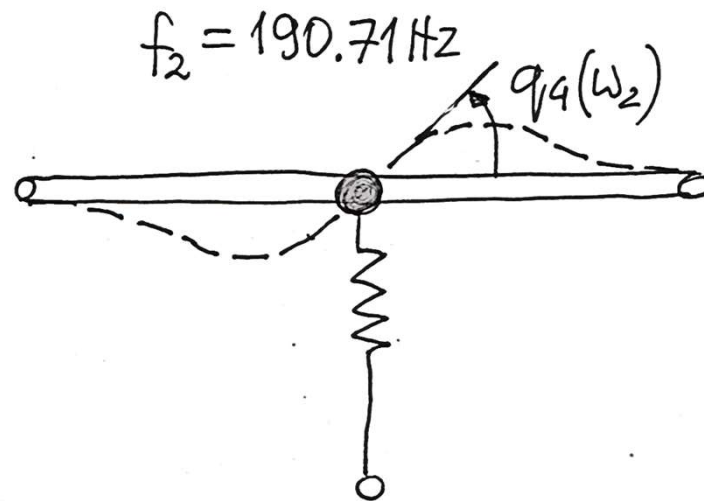


for  $\omega_2$  :  $\bar{\Phi}(\omega_2) \neq 0$  ,  $\bar{\Psi}(\omega_2) = 0$

$$\bar{\Phi}(\omega_2) \cdot \underbrace{q_3(\omega_2)}_{=0} + 0 \cdot q_4(\omega_2) = 0$$

$\hookrightarrow$  any real value

2nd vibration mode



b) for  $\omega_2$  Mass  $M_0$  only rotates :

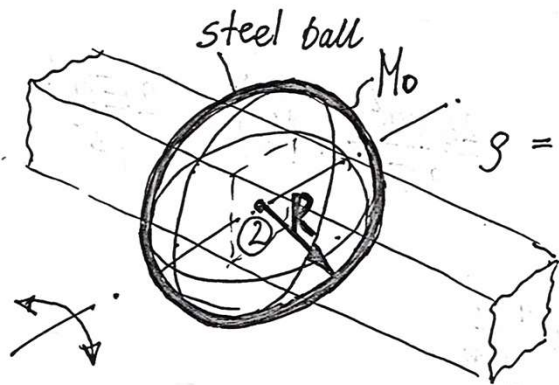
$$\tilde{\omega}_1^2 > \omega_2^2$$

$$\frac{\frac{2Ea^4}{l^3} + \tilde{k}}{\frac{26 \rho a^2 l}{35} + M_0} > \frac{35Ea^2}{\rho l^4}$$

$$\tilde{k} > \frac{35Ea^2}{\rho l^4} \cdot \left( \frac{26 \rho a^2 l}{35} + M_0 \right) - \frac{2Ea^4}{l^3}$$

$$\tilde{k} > 4.1 \cdot 10^4 \frac{N}{mm}$$

if the moment of inertia is considered :



$$\rho = \frac{M_0}{V} = \frac{3M_0}{4\pi R^3} \Rightarrow R = \sqrt[3]{\frac{3M_0}{4\pi \rho}} = 85 \text{ mm}$$

$$J_0 = \frac{2}{5} M_0 \cdot R^2 = \frac{2}{5} \cdot 0.02 \frac{\text{Ns}^2}{\text{mm}} \cdot 85^2 \text{ mm}^2 = 57.8 \text{ Ns}^2 \text{ mm}$$

$$[m']_4^* = \begin{bmatrix} 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & M_0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & J_0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 \end{bmatrix}$$

$$\omega_2' = \sqrt{\frac{\frac{2Ea^4}{3L}}{\frac{2\rho a^2 L^3}{105} + J_0}} = 1074.7 \text{ } 1/s$$

$$f_2' = 171 \text{ Hz}$$

$$K_2' > \frac{\frac{2Ea^4}{3L}}{\frac{2\rho a^2 L^3}{105} + J_0} \left( \frac{26\rho a^2 L}{35} + M_0 \right) - \frac{2Ea^4}{L^3}, \quad K_2' > 3.28 \cdot 10^9 \frac{\text{N}}{\text{mm}}$$